



**Project:** Mr. & Mrs. Friedman's Residence,  
**Location:** Windmill Lake Estates, Weston, Florida

This report provides full structural calculations of the building elements to be built at the above referenced address. This new residence has approximate total area of 8600 ft<sup>2</sup> of which approximate 1250 ft<sup>2</sup> is a second floor. Details of these calculations are documented in the enclosed A-H exhibits as follows:

**Exhibit A:** Wind Calculations for Main Wind Force Resisting System & Components and Claddings

**Exhibit B:** Truss and Girder loading, Connectors to Structure, & Foundation Loading.

**Exhibit C:** Concrete Masonry Unit Typical cross sections.

**Exhibit D:** Wood Frame Wall and Wood Posts

**Exhibit E:** Concrete Beams

**Exhibit F:** Steel Posts

**Exhibit G:** Foundation

**Exhibit H:** Shear Wall Analysis

SEAL

**Consulting Engineer  
AL ALI, PhD PE 53318**

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**Mr. & Mrs. Friedman's Residence, Windmill Lake Estates, Weston, Florida**



Exhibit A

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Velocity Pressure Calculations, qz (Cont.)						
Where :	Kh	=	Velocity pressure coefficient @ height z	(Eq. C6-4a)		
		=	$2.01 \cdot (z/Zg) ^ {2/\alpha}$ for $15 \text{ ft} \leq Z \leq Zg$	(Eq. C6-4b)		
		=	$2.01 \cdot (15/Zg) ^ {2/\alpha}$ for $Z < 15 \text{ ft}$			
		=	0.97155			
	Kzt	=	Topographic factor obtained from Fig. 6-4			
	Kzt @ h	=				
	Topography	=	None			
	K1,K2,K3	=	None			
	Lh	=	Roof Leeward Exposure Obtain Kzt			
	H	=				
	H/Lh	=				
	K1	=				
	X	=				
	X/Lh	=				
	K2	=				
	z/Lh	=				
	K3 @ h	=				
	Kd	=	Windward Exposure Coefficient obtained from Table 6-4			
	qh	=				
Internal Pressure Coefficient, GCpi, Figure 6-5						
The internal pressure coefficients are given in Figure 6-5						
Enclosure Classification	GCpi+	GCpi-	Ri	GCpi+	GCpi-	
Enclosed Buildings	0.18	-0.18		0.18	-0.18	



Velocity Pressure Calculations, qz (Cont.)						
Where :	$K_h$	=	Velocity pressure coefficient @ height z	(Eq. C6-4a)		
		=	$2.01 \cdot (z/Z_g)^\alpha$ for $15 \text{ ft} \leq Z \leq Z_g$	(Eq. C6-4b)		
		=	$2.01 \cdot (15/Z_g)^\alpha$ for $Z < 15 \text{ ft}$			
		=	0.990705			
	$K_{zt}$	=	Topographic factor obtained from Fig. 6-4			
	$K_{zt} @ h$	=				
	Topography $K_1, K_2, K_3$	=	None. Obtain $K_{zt}$			
	$L_h$					
	$H$					
	$H/L_h$					
	$K_1$					
	$X$					
	$X/L_h$					
	$K_2$					
	$z/L_h$					
	$K_3 @ h$					
	$K_d$	=	Wind directionality factor obtained from Table 6-4			
	$q_h$	=				
Internal Pressure Coefficient, $G_{Cpi}$ , Figure 6-5						
The internal pressure coefficients are given in Figure 6-5						
Enclosure Classification	$G_{Cpi+}$	$G_{Cpi-}$	$R_e$	$G_{Cpi+}$	$G_{Cpi-}$	
Enclosed Buildings	0.18	-0.18		0.18	-0.18	



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Exhibit B

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Connector	All. Uplift (#)	All. F1 (#)	All. F2 (#)	Design OK?
AB1	3350	1225	1520	
Is force independent?		NO	NO	
<b>Ratio (Lt/Ft)</b>	<b>0.44</b>	<b>0.65</b>	<b>0.89</b>	<b>OK</b>
			<b>0.82</b>	<b>OK</b>

Case1  
Case 2

Foundation			
Load for Foundation lb/ft			2,508.1
Required length of 1' Ftg. (inches)			12.0

Monolithic

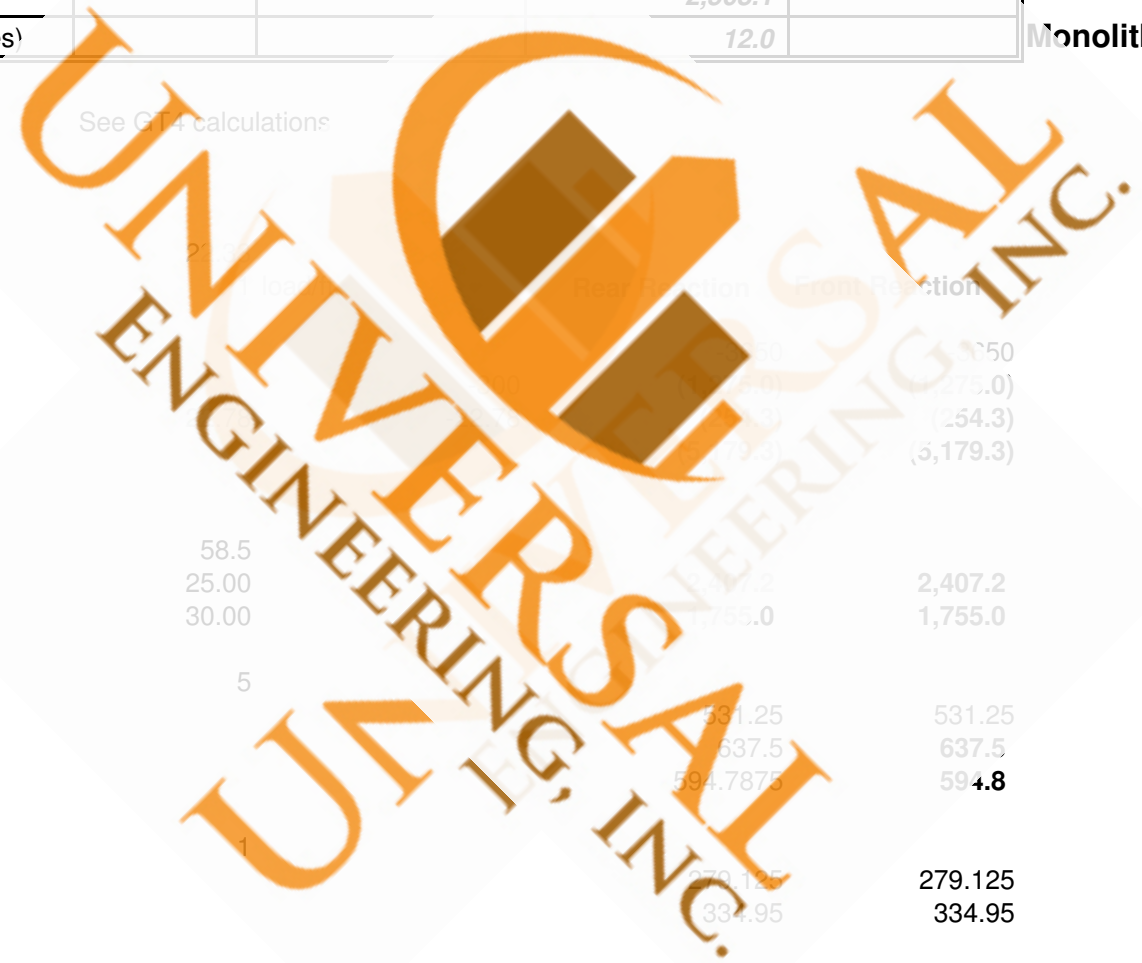
**GT3**

See GT4 calculations

**GT4**

Span  
Tributary area

conc. Load from above  
Uniform over 8.5 ft.  
uplift  
**UPLIFT**  
DL  
conc. Load from above  
tributary area per corner  
DL  
LL  
uniform load from above  
average tributary area  
reaction on each end, DL  
reaction on each end, LL  
DL of wall  
uniform load from first roof  
average tributary area  
reaction on each end  
  
Conc. Load  
DL @  
LL @



	Span	Tributary area	DL	LL	DL of wall	DL @	LL @	Reaction
	10.0	42.5	2050	2750	594.7875	9.5	9.5	(3,179.3)
			58.5	25.00	594.7875	9.5	9.5	2,407.2
			30.00	30.00	594.7875	9.5	9.5	1,755.0
	5		531.25	637.5	594.7875	9.5	9.5	531.25
			531.25	637.5	594.7875	9.5	9.5	637.5
			594.7875	637.5	594.7875	9.5	9.5	594.8
	1		279.125	334.95	594.7875	9.5	9.5	279.125
			279.125	334.95	594.7875	9.5	9.5	334.95
			807.5	969	594.7875	9.5	9.5	807.5
			807.5	969	594.7875	9.5	9.5	969.0



Truss ID	Uplift (lbs)	DL (lbs)	LL (lbs)	TL (lbs/ft)	TL (lbs)	Founda	F1 int (Ft)	F2 int (L/Ft)	OK?	INT	OK?	
T01	495	150	180	18	18		0.88	0.89	OK	1.13	OK	
T02	540	200	240	18	18		0.91	0.92	OK	1.15	OK	
T03	372	150	180	18	18		0.82	0.82	OK	1.08	OK	
T04	1190	913	1095	18	18		0.75	0.94	OK	1.26	OK	
T05	785	469	585	18	18		0.85	0.85	OK	1.25	OK	
T06	852	542	650	18	18		0.95	0.94	OK	1.26	OK	
T07	1030	738	885	18	18		0.97	0.94	OK	1.26	OK	
T08	678	336	403	18	18		0.99	0.99	OK	1.20	OK	
T09	767	439	527	40	40		1.04	1.04	OK	1.24	OK	
T10	638	449	538	494	494		0.97	0.97	OK	1.19	OK	
T11	398	194	233	214	214		0.44	0.87	OK	0.81	OK	
T12	429	227	272	250	250		0.85	0.85	OK	1.10	OK	
T13	658	313	375	344	10.7		0.58	1.01	OK	0.92	OK	
T14	563	225	270	248	980		0.93	0.93	OK	1.16	OK	
T15	609	275	330	303	1035		0.95	0.95	OK	1.18	OK	
T16	1064	775	930	853	1585	MONO	0.75	0.94	OK	1.26	OK	
T17	761	442	530	486	1218	MONO	0.75	0.94	OK	1.26	OK	
T18	780	463	555	509	1241	MONO	0.25	1.09	OK	1.01	OK	
GT16	1364	590	708	649	853	MONO	D	0.75	0.99	OK	0.90	OK
GT17	780	463	555	509	631	MONO	D	0.52	0.76	OK	0.72	OK
GT18	2793	903	1083	993	1430	MONO	KA	0.46	0.70	OK	0.57	OK



**Mr. & Mrs. Friedman's Residence, Windmill Lake Estates, Weston, Florida**



Exhibit C

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Universal Engineering, Inc.

Short Period Spectral Acceleration,  $S_s = 0.00 \%$   
 One Second Spectral Acceleration,  $S_1 = < 0.75 g$   
 (Computed) Design Category,  $= \text{Category A}$   
 Parapet Component Importance Factor,  $I_p = 1$   
 Parapet Height/Roof Height Ratio  $z/h = 0$   
 Veneer weight  $= 0.00 \text{ psf.}$   
 Seismic Load on Main wall\*  $= 5.50 \text{ psf.}$   
 \* Minimum Code Required Value  
 Seismic Load on Parapet wall  $= 0.00 \text{ psf.}$

Masonry wall: MASONRY WALL ANALYSIS AND DESIGN

Project : Friedman  
 Location: Weston, Florida

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WIND LOADS:

	Load W or H	Magni Coeff	Distri Coeff
1	W		
2			
3			
4			
5			

- Notes: 1. "W" designates a windward wind load.  
 "H" designates a leeward wind load.  
 2. Horizontal loads are in the direction of wind load.

MASONRY DATA:

Masonry Unit Strength  $= 19 \text{ psi.}$   
 Masonry Compressive Strength,  $f'_m = 1500 \text{ psi.}$   
 Allowable Flexural Stress,  $F_b = 500.00 \text{ psi.}$   
 Allowable Shear Stress,  $F_v = 38.73 \text{ psi.}$   
 Allowable Tension: No Grout,  $F_t = 25.00 \text{ psi.}$   
 Solid Grout,  $F_t = 68.00 \text{ psi.}$   
 Modulus of Elasticity,  $E_m = 1,350 \text{ ksi.}$   
 Modular Ratio,  $E_s/E_m = n = 21.48$   
 Single Grouted Cell + web width  $= 8.00 \text{ in.}$   
 Nominal Length of Masonry Unit  $= 16.00 \text{ in.}$   
 Block Face Shell Thickness  $= 1.25 \text{ in.}$   
 Nominal Minus Actual Thickness  $= 0.38 \text{ in.}$

MATERIAL DATA:

Universal Engineering, Inc.

Steel Yield Strength,  $F_y = 60.00$  ksi.  
Allowable Steel Stress,  $F_s = 24.00$  ksi.  
Modulus of Elasticity,  $E_s = 29,000$  ksi.

REINFORCED WALL DATA:

Minimum Steel Ratio,  $A_s/bt = 0.0007$

Masonry wall: MASONRY WALL ANALYSIS AND DESIGN

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DESIGN LOADS:

Moment,  $M = 12.00$  ft-kip  
Axial Load,  $P = 0.00$  kip  
Load Combination  
Eccentricity at Moment,  $e = M/P$

NOTE: Max. moment is located in Zone 1  
wall is cracked, steel is stressed

Max. Shear,  $V_s = 216.00$  lb  
Load Combination  
 $= 0.6 * D$

ANALYSIS RESULTS:

Design Strip width = 12.00 in.  
Actual wall Thickness,  $t = 7.63$  in.  
Effective Height,  $h' = 12.00$  ft.  
Seismic Force, (IBC 2000 1620.1.7)  $F_p = 5.50$  plf. / 12.00 in.  
Minimum Area of Steel, Vertical Reinf. = 0.064 in.<sup>2</sup> / 12.00 in.  
Minimum Area of Steel, Horiz. Reinf. = Not Required

Ref. ACI 99 1.11/IBC 2000 2109.6.5

DESIGN RESULTS:

All. Moment

Universal Engineering, Inc.

6	4.80	622.1	1,400.0	43.2
7	3.60	544.3	1,466.0	86.4
8	2.40	414.7	1,532.0	129.6
9	1.20	233.3	1,598.0	172.8
10	0.00	0.0	1,664.0	216.0

WALL PROPERTIES:

Effective Flange Width	bf = 10.29 in. / 12.00 in.
Effective Grouted Core Width,	b' = 1.71 in. / 12.00 in.
Solid Masonry Area,	Ae = 34.50 in. <sup>2</sup> / 12.00 in.
Gross Moment of Inertia,	Ig = 283.84 in. <sup>4</sup> / 12.00 in.
Section Modulus,	S = 2*Ig/t = 74.45 in. <sup>3</sup> / 12.00 in.
Radius of Gyration,	r = 2.868 in. / 12.00 in.
Slenderness Factor,	h'/r = 50.20

ALLOWABLE STRESSES:

Allowable Axial Stress,	fa = 666.67 psi.
Allowable Bending Stress,	fb = 666.67 psi.
Allowable Shear Stress,	fv = 21.64 psi.
Allowable Steel Stress,	fs = 20,000 psi.

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 Location: Weston, MA  
 Designer: [Redacted] PhD, PE # 53318

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DETAILED RESULTS FOR MAIN WALL

LOAD COMBINATION : 1\*DL+1\*LL  
 REBAR DESIGN : #5 @ 56 in.  
 FURNISHED AREA OF STEEL : 0.066 in<sup>2</sup>  
 MINIMUM AREA OF STEEL : 0.064 in<sup>2</sup>

No.	Dist From Bot (ft)	Mom. (ft-lb)	Axial (lbs)	Shear (lbs)
0	12.00	0.0	1,004.0	-23.1
1	10.80	24.9	1,070.0	-18.5
2	9.60	44.4	1,136.0	-13.9
3	8.40	58.2	1,202.0	-9.2
4	7.20	66.5	1,268.0	-4.6
5	6.00	69.3	1,334.0	0.0
6	4.80	66.5	1,400.0	4.6
7	3.60	58.2	1,466.0	9.2
8	2.40	44.4	1,532.0	13.9
9	1.20	24.9	1,598.0	18.5
10	0.00	0.0	1,664.0	23.1

Universal Engineering, Inc.

Short Period Spectral Acceleration,  $S_s = 0.00 \%$   
 One Second Spectral Acceleration,  $S_1 = < 0.75 g$   
 (Computed) Design Category,  $= \text{Category A}$   
 Parapet Component Importance Factor,  $I_p = 1$   
 Parapet Height/Roof Height Ratio  $z/h = 0$   
 Veneer weight  $= 0.00 \text{ psf.}$   
 Seismic Load on Main wall\*  $= 5.50 \text{ psf.}$   
 \* Minimum Code Required Value  
 Seismic Load on Parapet wall  $= 0.00 \text{ psf.}$

Masonry wall: MASONRY WALL ANALYSIS AND DESIGN

Project : Friedman  
 Location: Weston, Florida

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WIND LOADS:

	Load W or H	Magni (Coeff)	Distri (Coeff)
1	W		
2			
3			
4			
5			

Notes: 1. "W" designates a windward wind load.  
 "H" designates a horizontal wind load.  
 2. Horizontal loads are based on the wind load.

MASONRY DATA:

Masonry Unit Strength  $= 1500 \text{ psi.}$   
 Masonry Compressive Strength,  $f'_m = 1500 \text{ psi.}$   
 Allowable Flexural Stress,  $F_b = 500.00 \text{ psi.}$   
 Allowable Shear Stress,  $F_v = 38.73 \text{ psi.}$   
 Allowable Tension: No Grout,  $F_t = 25.00 \text{ psi.}$   
 Solid Grout,  $F_t = 68.00 \text{ psi.}$   
 Modulus of Elasticity,  $E_m = 1,350 \text{ ksi.}$   
 Modular Ratio,  $E_s/E_m = n = 21.48$   
 Single Grouted Cell + web width  $= 8.00 \text{ in.}$   
 Nominal Length of Masonry Unit  $= 16.00 \text{ in.}$   
 Block Face Shell Thickness  $= 1.25 \text{ in.}$   
 Nominal Minus Actual Thickness  $= 0.38 \text{ in.}$

MATERIAL DATA:

Universal Engineering, Inc.

Bar Size	Fa, psi (4/3*.25*f'm*R)	fv, psi (V/b'd)	@ Axial Load (P=955.5 lb)	Bar Spa. (in. o.c.)
#3	448.34	7.34	1,037.2	16.00
#4	457.62	14.68	970.8	32.00
#5	461.13	25.69	888.8	56.00
#6	461.13	33.03	915.3	72.00
#7	461.13	33.03	1,003.7	72.00
#8	461.13	33.03	1,081.0	72.00
#9	461.13	33.03	1,144.5	72.00

Max. vertical bar spacing is 72 inch per ACI 99 2.3.3.3 (commentary)  
 Per IBC 2000 2107.2.4, bar size is limited to #8

Masonry wall: MASONRY WALL ANALYSIS AND DESIGN

Project : Friedman  
 Location: Weston, Florida

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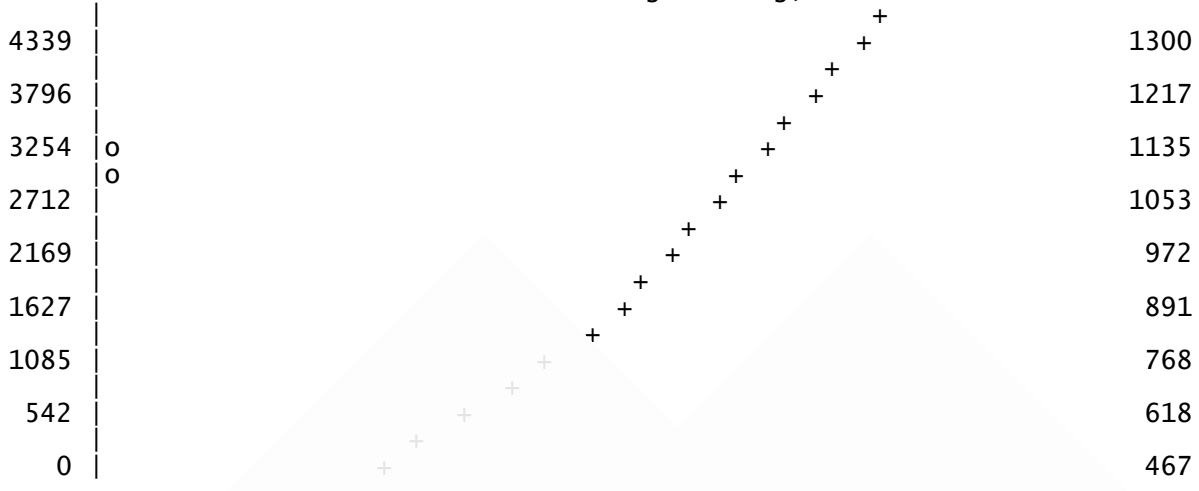
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MASONRY WALL INTERACTION (ACI 530-11 ONLY)

Effective wall Height = 11.93 ft       $A_e = 50 \text{ in}^2$   
 Actual wall Thickness = 16 in       $F_a = 457.62 \text{ psi}$   
 Depth to c.g. Section = 8 in       $F_v = 33.03 \text{ psi}$   
 Design width = 16 in       $F_p = 1000 \text{ ksi}$   
 Reinforcing Design

Axial	Moment
11932	956
11389	1054
10847	1151
10305	1249
9762	1346
9220	1444
8678	1542
8135	1625
7593	1674
7051	1656
6508	1606
5966	1533
5424	1460
4881	1381





NOTES: Axial Load = Lb, Moment = ft-lb  
 + = Moment Capacity  
 o = Applied Moment

Positive moment is defined as moment which causes compression on the outside face of wall.

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MASONRY WALL INTERACTION DIAGRAM (STRESS IN PSI)

Effective wall Height = 9.33 ft. Gross Area,  $A_g = 34.50 \text{ in}^2$   
 Actual wall Thickness = 7.63 in. Stress,  $F_a = 461.13 \text{ psi}$   
 Depth to c.g. Steel = 3.81 in. Stress,  $F_b = 666.67 \text{ psi}$   
 Design width = 12.00 in. Allow. Stress,  $F_s = 32.00 \text{ ksi}$   
 Reinforcing Design = #5 @ 56 in. o.c.







**Mr. & Mrs. Friedman's Residence, Windmill Lake Estates, Weston, Florida**



Exhibit D

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**Timber Design 1 - Option 1 - Design of Member 1 - 2x6** ✓🇺🇸

**Design Data**

Design of Member 1 - 2x6 ✓		
Material type is No. 2 -Southern Pine -Dimensional		
Check for repetitive use? No	Top flange bracing is Fully Braced	E <sub>bx</sub> : 1.6e+06 psi
Moist use? No	Bottom flange bracing is Fully Braced	E <sub>by</sub> : 1.6e+06 psi
I <sub>x</sub> = 20.8 in <sup>4</sup> S <sub>x</sub> = 7.6 in <sup>3</sup>	I <sub>y</sub> = 1.5 in <sup>4</sup> S <sub>y</sub> = 2.1 in <sup>3</sup>	G assumed as .06E
Shear C <sub>H</sub> = 1 Snow C <sub>s</sub> = 1.15	This is not a tapered column	1250 psi
Side loaded? No	K <sub>x</sub> = 1	psi
Overstress factor = 1	L <sub>u</sub> = 0	psi
Allowable Floor live load deflection = L/360	L <sub>u</sub> = 0	psi
Allowable Floor total load deflection = L/240 (S in Maximum)	L <sub>u</sub> = 0	psi
Member weight used in analysis = 0 plf	Area = 0	psi

**Critical Design**

	Critical Reaction lb			
Span 1 Value	392			0.269
Allowable	1271.33	N/A		0.4667
% of Allow.	31 ✓	0 ✓		57 ✓
Location	0'	5'3"	11'-0"	4'11-3/32"

	C <sub>D</sub>	C <sub>t</sub>	C <sub>L</sub>	C <sub>v</sub>	C <sub>fu</sub>	C <sub>Py</sub>	C <sub>H</sub>	C <sub>T</sub>
Span 1	1.600	1.000	1.000	1.000	1.000	1.000	1.000	1.000

	C <sub>b</sub>	C <sub>Fb</sub>	C <sub>Ft</sub>	C <sub>FE</sub>	C <sub>mb</sub>	C <sub>mo</sub>	C <sub>M1</sub>	C <sub>Mc</sub>	C <sub>ME</sub>	R <sub>b</sub>
Span 1	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	0

	L/d Limit	L <sub>x</sub> /d	L <sub>y</sub> /d	F <sub>CE x</sub> psi	F <sub>CE y</sub> psi	F <sub>BE</sub> psi	K <sub>CE</sub>	c	F <sub>c</sub> psi
Span 1	50	20.36	74.67	1157.53	36.0969	1e+06	0.3	0.8	2560

**Notes:**

- Member has an actual/allowable ratio in span 1 of 86 ✓%.
- Design is governed by live load deflection.

- Governing load combination is Dead+Wind in Neg X.
- Maximum hanger forces: 392 lb (Left) and -304.889 lb (Right).

## Minimum Bearing

<i>Span</i>	<i>Actual Length</i> <i>ft</i>	<i>Left Support Min. Bearing</i> <i>in</i>	<i>Right Support Min. Bearing</i> <i>in</i>
Span 1	9'4"	1.5	1.5

### Notes:

- Locations of maximum stress, moment, etc are measured from the left end of the member.
- Bearing across full width of beam is required.
- Structural adequacy of supporting members must be confirmed.
- Bearing lengths required may be varied by limiting stress on supporting members.
- A negative reaction indicates that the beam is required to the support to resist uplift.
- See manufacturer's literature for additional requirements.
- Cantilever deflection at ends is allowed over the span length.
- Timber design if applicable.

- Governing load combination is Dead+Roof Live.
- Axial capacity of member is 3203.75 lb.
- Maximum hanger forces: 261.333 lb (Left) and 261.333 lb (Right).

## Minimum Bearing

<i>Span</i>	<i>Actual Length</i> <i>ft</i>	<i>Left Support Min. Bearing</i> <i>in</i>	<i>Right Support Min. Bearing</i> <i>in</i>
Span 1	9'4"	1.5	1.5

### Notes:

- Locations of maximum stress, moment, etc. are measured from the left end of the member.
- Bearing across full width of beam is required.
- Structural adequacy of supporting members must be confirmed.
- Bearing lengths required may be dictated by design on supporting members.
- A negative reaction indicates that the support is required to resist uplift.
- See manufacturer's literature for additional requirements.
- Cantilever deflection allowed is 1/160 of the span length.
- Timber design is required by code.



**Mr. & Mrs. Friedman's Residence, Windmill Lake Estates, Weston, Florida**



Exhibit E

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=====
# 1 Concentrated Load:      3.700 K           3.330 K
      Distance:              4.330 Ft          4.330 Ft

# 2 Concentrated Load:      0.780 K           0.940 K
      Distance:              3.000 Ft          3.000 Ft

# 1 Uniform Load:           0.120 K /Ft         0.140 K /Ft
      Distance to Begin:     0.000 Ft          0.000 Ft
      Distance to End:       6.000 Ft          6.000 Ft
  
```

```

# 2 Uniform Load:           0.094 K /Ft         0.113 K /Ft
      Distance to Begin:     0.000 Ft          0.000 Ft
      Distance to End:       3.200 Ft          6.000 Ft

# 3 Uniform Load:           0.200 K /Ft         0.070 K /Ft
      Distance to Begin:     0.000 Ft          0.000 Ft
      Distance to End:       6.000 Ft          6.000 Ft
  
```

		C R I T I C A L S H E A R S & M O M E N T S				
		DEAD LOAD	LOAD COMB 1	LOAD COMB 2	LOAD COMB 3	LOAD
<hr/>						
COMB 4						
<hr/>						
Load Combination Dead Load:						
Load Combination # 1:						
Load Combination # 2:						
Load Combination # 3:						
Load Combination # 4:						
<hr/>						
Shear	Left End:					
5.276 K						
Moment	Left End:					
0.000 K -Ft						
Shear	Right End:					
8.553 K						
Moment	Right End:					
0.000 K -Ft						
Maximum Moment	:	-8.553 K -Ft				
13.395 K -Ft	Located at:	4.330 Ft				
4.330 Ft						
Max Deflection	:	0.072 In				
0.167 In	Located at:	3.169 Ft				
3.174 Ft						
Dead Part:		0.072 In				
0.072 In						
Inflection Points:		0.000 Ft				
0.000 Ft						
6.000 Ft						
6.000 Ft						
Reaction	Left End:	-3.641 K				
5.276 K						
Reaction	Right End:	-5.741 K				
8.553 K						

C R I T I C A L S H E A R S & M O M E N T S



Load Combination # 5: 1.200 x Dead Load + 1.000 x L + 1.400 x E + 0.200 x R  
 Load Combination # 6: 0.900 x Dead Load + 1.600 x W  
 Load Combination # 7: 0.900 x Dead Load + 1.400 x E  
 Load Combination # 8: 1.200 x Dead Load - 0.800 x W + 1.600 x R  
 Load Combination # 9: 1.200 x Dead Load + 1.000 x L - 1.600 x W + 0.500 x R

Shear	Left End:	-5.276 K	-2.340 K	-2.340 K	-3.121 K	-
5.276 K						
Moment	Left End:	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	-
0.000 K -Ft						
Shear	Right End:	8.553 K	3.690 K	3.690 K	4.920 K	-
8.553 K						
Moment	Right End:	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	-
0.000 K -Ft						
Maximum Moment	:	-13.395 K -Ft	-5.761 K -Ft	-5.761 K -Ft	-7.682 K -Ft	-
13.395 K -Ft						
Located at:		4.330 Ft	3.330 Ft	3.330 Ft	4.330 Ft	-
4.330 Ft						
Max Deflection	:	0.167 In	0.072 In	0.072 In	0.072 In	-
0.167 In						
Located at:		3.174 Ft	3.169 Ft	3.169 Ft	3.169 Ft	-
3.174 Ft						
Dead Part:		0.072 In	0.072 In	0.072 In	0.072 In	-
0.072 In						
Inflection Points:		0.000 Ft	0.000 Ft	0.000 Ft	0.000 Ft	-
0.000 Ft						
		6.000 Ft	6.000 Ft	6.000 Ft	6.000 Ft	-
6.000 Ft						
Reaction	Left End:	-5.276 K	-2.340 K	-2.340 K	-3.121 K	-
5.276 K						
Reaction	Right End:	8.553 K	3.690 K	3.690 K	4.920 K	-
8.553 K						

Load Combination #10: 1.200 x Dead Load + 1.000 x L + 1.400 x E + 0.200 x R  
 Load Combination #11: 0.900 x Dead Load + 1.600 x W  
 Load Combination #12: 0.900 x Dead Load + 1.400 x E

Shear	Left End:	-5.276 K	-2.340 K	-2.340 K	-3.121 K	-
5.276 K						
Moment	Left End:	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	-
0.000 K -Ft						
Shear	Right End:	8.553 K	3.690 K	3.690 K	4.920 K	-
8.553 K						
Moment	Right End:	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	-
0.000 K -Ft						
Maximum Moment	:	-13.395 K -Ft	-5.761 K -Ft	-5.761 K -Ft	-7.682 K -Ft	-
13.395 K -Ft						
Located at:		4.330 Ft	3.330 Ft	3.330 Ft	4.330 Ft	-
4.330 Ft						
Max Deflection	:	0.167 In	0.072 In	0.072 In	0.072 In	-
0.167 In						
Located at:		3.174 Ft	3.169 Ft	3.169 Ft	3.169 Ft	-
3.174 Ft						
Dead Part:		0.072 In	0.072 In	0.072 In	0.072 In	-
0.072 In						
Inflection Points:		0.000 Ft	0.000 Ft	0.000 Ft	0.000 Ft	-
0.000 Ft						
		6.000 Ft	6.000 Ft	6.000 Ft	6.000 Ft	-
6.000 Ft						
Reaction	Left End:	-5.276 K	-2.340 K	-2.340 K	-3.121 K	-
5.276 K						
Reaction	Right End:	8.553 K	3.690 K	3.690 K	4.920 K	-
8.553 K						



Shear	Left End:	9.931 K	4.532 K	4.532 K	6.043 K	
9.931 K						
Moment	Left End:	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	
0.000 K -Ft						
Shear	Right End:	-9.931 K	-4.532 K	-4.532 K	-6.043 K	-
9.931 K						
Moment	Right End:	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	
0.000 K -Ft						
Maximum Moment	:	43.868 K -Ft	20.022 K -Ft	20.022 K -Ft	26.696 K -Ft	
43.868 K -Ft						
Located at:		8.835 Ft	8.835 Ft	8.835 Ft	8.835 Ft	
8.835 Ft						
Max Deflection	:	-0.042 In	-0.024 In	-0.024 In	-0.024 In	-
0.042 In						
Located at:		8.835 Ft	8.835 Ft	8.835 Ft	8.835 Ft	
8.835 Ft						
Dead Part:		-0.024 In	-0.024 In	-0.024 In	-0.024 In	-
0.024 In						
Inflection Points:		0.000 Ft	0.000 Ft	0.000 Ft	0.000 Ft	
0.000 Ft						
Located at:		17.670 Ft	17.670 Ft	17.670 Ft	17.670 Ft	
17.670 Ft						
Reaction	Left End:	9.931 K	4.532 K	4.532 K	6.043 K	
9.931 K						
Reaction	Right End:	9.931 K	4.532 K	4.532 K	6.043 K	
9.931 K						

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SECTION DESIGN INFORMATION

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Load Combination	#10:					
Load Combination	#11:					
Load Combination	#12:	0.				

Shear	Left End:	9.931 K	4.532 K	4.532 K	6.043 K
Moment	Left End:	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft
Shear	Right End:	-9.931 K	-4.532 K	-4.532 K	-6.043 K
Moment	Right End:	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft	0.000 K -Ft
Maximum Moment	:	43.868 K -Ft	20.022 K -Ft	20.022 K -Ft	26.696 K -Ft
Located at:		8.835 Ft	8.835 Ft	8.835 Ft	8.835 Ft
Max Deflection	:	-0.042 In	-0.024 In	-0.024 In	-0.024 In
Located at:		8.835 Ft	8.835 Ft	8.835 Ft	8.835 Ft
Dead Part:		-0.024 In	-0.024 In	-0.024 In	-0.024 In
Inflection Points:		0.000 Ft	0.000 Ft	0.000 Ft	0.000 Ft
Located at:		17.670 Ft	17.670 Ft	17.670 Ft	17.670 Ft
Reaction	Left End:	9.931 K	4.532 K	4.532 K	6.043 K
Reaction	Right End:	9.931 K	4.532 K	4.532 K	6.043 K



**Mr. & Mrs. Friedman's Residence, Windmill Lake Estates, Weston, Florida**



Exhibit F

**UNIVERSAL ENGINEERING, INC.** CA: 26583  
12828 Buckland St., West Palm Beach, FL 33414  
Tel: (561) 204-5000, Fax: (561) 204-1050,  
Web: [www.uefirm.com](http://www.uefirm.com); Email: [info@uefirm.com](mailto:info@uefirm.com)

**AL ALI, PhD, PE 53318**

## Steel Column Check SC1

Element: **SC1**  
 Description: Steel Column with worst loading conditions  
 Date: **10/24/2009 01:02 PM**  
 Design

Company: **Universal Engineering, Inc.**  
 User: **Dr. AL ALI**  
 Software: **Digital Canal Steel Beam Column**

### GENERAL INFORMATION

Description	Value	Description	Value
Run Mode	Check Mode	$K_y$	1.00
Design Code	AISC AISC 360	$K_z$	1.00
Beam-Column Length	12.00	Translation Deflection Limit	$L / 240$
Steel Yield Stress	50.00	Displacement Deflection Limit	$L / 360$
$C_b$ Calculation	$1.75 + 1.0$	Unbraced (LTB) Length	
$C_{mx}$ Calculation			
$C_{mz}$ Calculation			
$L_x$			
$L_y$			
$L_z$			
$K_x$			TS3.5x3.5x.25

### LOAD INFORMATION

Ref. No.	Load Case	Load Type	Begin Position	End Value	End Position
1	Dead	Concen	Z	-	-
2	Live	Concen	Z	-	-
3	Wind	Concen	Z	-	-

### SELECTED LOAD COMBINATIONS

Load Combination	Dead	Live	Dependent	Conditional
LC1: 1.0DL+1.0LL+1.0WL+1.0SL				X
LC2: 1.4DL			X	
LC3: 1.2DL+1.6LL+0.5SL			X	
LC4: 1.2DL+1.6SL+0.5LL	X		X	
LC5: 1.2DL+1.6SL+0.8WL	X		X	
LC6: 1.2DL+1.3WL+0.5LL+0.5SL	X		X	
LC7: 1.2DL+0.5LL+0.2SL	X		X	

### CRITICAL STRESS SUMMARY

Ref. No.	Section Name	Status	Governing Criteria	Stress Ratio	Load Combination	Distance (ft)





**Mr. & Mrs. Friedman's Residence, Windmill Lake Estates, Weston, Florida**



Exhibit G

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**AL ALI, PhD, PE 53318**



## MF1

Based on loadings in Exhibit B, use 16"X18", 2#5 bottom and 1 #5 top

## MF2

Based on loadings in Exhibit B, use 16"X24", 3#5 bottom and 1 #5 top

## MF3

Based on loadings in Exhibit B, use 16"X24", 3#5 bottom and 1 #5 top

## F3

Based on loadings in Exhibit B, for locations receiving less than 18 kips. Use 3 ft. X 3ft. X 16", 5#5 each way

## F3.5

Based on loadings in Exhibit B, for locations receiving less than 20 kips but more than 18 kips. Use 3 ft. X 3ft. X 16", 5#5 each way

## SW-

Stepped edges @ 12" on all sides  
longitudinally

## TE-

Thickened edge for minimum 10" for each 10" thickness



**Mr. & Mrs. Friedman's Residence, Windmill Lake Estates, Weston, Florida**



Exhibit H

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